Sediment-Trap Efficiency of a Multiple-Purpose Impoundment, North Branch Rock Creek Basin, Montgomery County, Maryland, 1968-76

GEOLOGICAL SURVEY WATER-SUPPLY PAPER 2071



Sediment-Trap Efficiency of a Multiple-Purpose Impoundment, North Branch Rock Creek Basin, Montgomery County, Maryland, 1968-76

By W. J. HERB

GEOLOGICAL SURVEY WATER-SUPPLY PAPER 2071

Prepared in Cooperation with the U.S. Department of Agriculture Soil Conservation Service



UNITED STATES DEPARTMENT OF THE INTERIOR

CECIL D. ANDRUS, Secretary

GEOLOGICAL SURVEY

H. William Menard, Director

Library of Congress Cataloging in Publication Data Herb, William J.

Sediment-trap efficiency of a multiple-purpose impoundment, North Branch Rock Creek basin, Montgomery County, Maryland, 1968-76.

(Geological Survey Water-Supply Paper 2071)

Bibliography: p. 41

Supt. of Docs. no.: 1 19.13:2071

 Sediment control-Maryland-Bernard Frank, Lake.
 Sediment control-Maryland-North Branch Rock Creek watershed.
 United States Soil Conservation Service.
 Title.

III. Series: United States Geological Survey Water-Supply Paper 2071.

TC424.M3H47 627'.14 79-607969

CONTENTS

| Page | |
|---|---|
| Abstract | |
| Introduction | |
| Acknowledgments | |
| Basin characteristics affecting sediment yields | |
| Climate5 | |
| Geology and soils | |
| Physiography and topography | |
| Land use and land cover | |
| Hydraulic structure | |
| Streamflow | |
| Sediment | |
| | |
| Methodology | |
| Sediment inflow | |
| Suspended sediment | |
| Bedload24 | |
| Ungaged sediment yield24 | |
| Sediment outflow | |
| Effects of impoundment | |
| Storm runoff and sediment discharge | |
| Particle size | |
| Trap efficiency | |
| Summary and conclusions40 | |
| References 41 | |
| | |
| ILLUSTRATIONS | |
| | |
| Page | , |
| FIGURE 1. Map showing location of North Branch Rock Creek | |
| basin | |
| 2. Graph showing mean monthly precipitation at locations | |
| near the study area | |
| 3. Graph showing annual variations in basin land use and | |
| • • | |
| land cover, North Branch Rock Creek near Rockville, | |
| 1968-76, | |
| 4-7. Photographs showing: | |
| 4. Lake Bernard Frank (A) earth-fill dam, (B) emergency | |
| spillway, (C) concrete riser, and (D) concrete | |
| impact basin12 | |
| 5. Gaging station, North Branch Rock Creek near | |
| Rockville | |
| 6. Gaging station, North Branch Rock Creek near Norbeck 15 | |
| 7. Gaging station, Manor Run near Norbeck | |
| 111 | |

CONTENTS

| Figure | 8-9. | Graphs showing: | Page |
|---------------|--------|---|------|
| | | 8. Sediment-transport curves used to compute un- | |
| | | measured storm-period suspended-sediment loads | |
| | | for North Branch Rock Creek near Norbeck | 18 |
| | | 9. Sediment-transport curves used to compute un- | |
| | | measured storm-period suspended-sediment loads | |
| | | for Manor Run near Norbeck | 20 |
| | 10–11. | Photographs showing: | |
| | | 10. Channel of North Branch Rock Creek near Norbeck | 25 |
| | | 11. Location of pumping-sampler intake, North Branch | |
| | | Rock Creek near Rockville | 27 |
| | 12-19. | Graphs showing: | |
| | | 12. Hydrograph for stations in North Branch Rock | |
| | | Creek basin, storm of May 13-14, 1971 | 29 |
| | | 13. Instantaneous suspended-sediment load in North | |
| | | Branch Rock Creek basin, storm of May 13-14, | |
| | | 1971 | 30 |
| | | 14. Relation of sand, silt, and clay content of suspended | |
| | | sediment to water discharge, North Branch Rock | |
| | | Creek near Norbeck | 32 |
| | | 15. Relation of sand, silt, and clay content of suspended | 02 |
| | | sediment to water discharge, Manor Run near | |
| | | Norbeck | 33 |
| | | 16. Annual sediment inflow, Lake Bernard Frank, by | |
| | | water year | 25 |
| | | 17. Cumulative sediment inflow and outflow, Lake | |
| | | Bernard Frank, by water year | 36 |
| | | 18. Annual sediment inflow to Lake Bernard Frank per | |
| | | inch of runoff | 37 |
| | | 19. Trap efficiency as related to capacity-inflow ratio | |
| | | for normal ponded reservoirs and Lake Frank | 20 |
| | | for normal policed reservoirs and Lake Frank | 39 |
| | | | |
| | | | |
| | | | |
| | | | |
| | | TABLES | |
| | | | |
| | | | Page |
| F ABLE | 1. S | summary of recorded data at gaging stations in the North | |
| | | Branch Rock Creek basin | 4 |
| | 2. L | and use and land cover, in acres, in the North Branch | |
| | | Rock Creek basin, 1968-76 | 8 |
| | 3. A | altitude, capacity, and surface-area relationships of Lake | |
| | | Bernard Frank | 14 |
| | 4. A | annual discharges, in cubic feet per second-days, for gages | |
| | | in the North Branch Rock Creek basin 1968-76 | 16 |

| | | Page |
|--------------|--|------|
| Cable | 5. Estimated monthly discharge totals for 1972 water year compared to measured monthly discharges for Manor Run near Norbeck | 23 |
| | 6. Annual storm suspended-sediment inflows to Lake Bernard | 20 |
| | Frank from Manor Run and North Branch Rock Creek | 23 |
| | 7. Annual suspended-sediment yields for land use and land cover categories for Northwest Branch Anacostia River and North Branch Rock Creek basins | 25 |
| | 8. Annual suspended-sediment yields, in tons, for land use and land cover categories, and total annual sediment yields, in tons, for ungaged portion of North Branch Rock Creek basin, 1968-76 | 26 |
| | Particle-size distribution of suspended sediment in the North Branch Rock Creek basin | 31 |
| | 10. Annual sediment inflow and outflow, Lake Bernard | |
| | Frank, 1968-76 | 34 |
| | 11. Annual sediment yields from total drainage basin of Lake | |
| | Frank, 1968-76 | 38 |

CONVERSION FACTORS

| To convert inch-pound unit | Multiply by | To obtain metric units |
|--|-------------|---|
| Inch (in.) | 25.4 | Millimeter (mm) |
| Foot (ft) | 0.3048 | Meter (m) |
| Acre | 0.4047 | Hectare (ha) |
| Square mile (mi ²) | 2.590 | Square kilometer (km²) |
| Cubic foot (ft ³) | | Cubic meter (m ³) |
| Acre-foot (acre-ft) | 1234 | Cubic meter (m ³) |
| Cubic foot per second-day (ft ³ /s-d) | 2447 | Cubic meter (m³) |
| Ton | 0.9072 | Megagram (Mg) |
| Cubic foot per second (ft ³ /s) | 0.02832 | Cubic meter per second (m ³ /s) |
| Pound per cubic foot (lb/ft ³) | 16.02 | Kilogram per cubic meter (kg/m³) |
| Cubic foot per second per square mile | | Cubic meter per second per |
| [(ft ³ /s)/mi ²] | 0.01093 | square kilometer [(m³/s)/km²] |
| Ton per acre | 2.242 | Megagram per hectare (Mg/ha) |
| Ton per square mile (ton/mi²) ······ | 0.3503 | Megagram per square kilo- meter (Mg/km²) |
| Ton per acre per inch [(ton/acre)/in.] | 0.0883 | Megagram per hectare per millimeter [(Mg/ha)/mm] |

SEDIMENT-TRAP EFFICIENCY OF A MULTIPLE-PURPOSE IMPOUNDMENT, NORTH BRANCH ROCK CREEK BASIN, MONTGOMERY COUNTY, MARYLAND, 1968–76

By WILLIAM J. HERB

ABSTRACT

Lake Bernard Frank, a multiple-purpose reservoir in Montgomery County, Md., impounds runoff and sediment from 12.5 square miles of the upper North Branch Rock Creek basin. Sediment-trap efficiency was studied by the U.S. Geological Survey between 1967 and 1976.

Suspended-sediment inflow to the impoundment for unmeasured storm periods in 1968-76 was estimated from daily suspended-sediment transport curves. Bedload contribution was estimated by the Schoklitsch and Meyer-Peter and Muller bedload-transport equations. The sediment contribution for the 1.76-square-mile ungaged part of the basin was estimated from land use and land cover determinations derived from aerial photographs taken annually and land use and land cover sediment-yield relations.

The impoundment attenuated both streamflow peaks and instantaneous sediment loads. An instantaneous streamflow peak on North Branch Rock Creek was measured at 207 cubic feet per second per square mile above the impoundment, but, for the same storm, the peak downstream from the impoundment was only 7.0 cubic feet per second per square mile. For one storm, the maximum instantaneous suspended-sediment load was measured at 4,880 tons per day on North Branch Rock Creek upstream from the impoundment, while the maximum instantaneous suspended-sediment load below the reservoir was 33 tons per day.

Discharge-weighted percentages of sand, silt, and clay averaged 16, 50, and 34 for locations upstream from the impoundment and were zero, 16, and 84 below the reservoir.

From 1968 through 1976, about 136,000 tons of sediment was estimated to have entered the impoundment. Over the same years, 5,910 tons of sediment was measured to have left the impoundment. The measured trap efficiency was 96 percent, which closely agrees with the trap efficiency computed from the impoundment's capacity-inflow ratio.

INTRODUCTION

In the early 1960's, two Public Law 566 structures sponsored by the Montgomery Soil Conservation District, Maryland-National Capital Park and Planning Commission, and Montgomery County were constructed in the Upper Rock Creek watershed. The purposes served by these structures were flood control, sediment reduction, fish and wildlife development, and recreation (Montgomery County and others, 1962). One structure is on Rock Creek, and the second structure, impounding Lake Bernard Frank, is on the North Branch Rock Creek just upstream from its confluence with Rock Creek.

The U.S. Geological Survey, in cooperation with the U.S. Soil Conservation Service, began investigations of streamflow and sedimentation in the North Branch Rock Creek basin (fig. 1), Montgomery County, Md., in September 1967. The investigation was part of a national effort to determine the sediment-trap efficiency of floodwater-retarding structures. Daily streamflow and suspended-sediment data were collected immediately downstream from Lake Frank at the North Branch Rock Creek near Rockville gaging station (01647740) (fig. 1). Daily streamflow and storm-period suspended-sediment data were collected at two upstream gaging stations in conjunction with a separate, but concurrent, research project in the same basin. Upstream data were collected for the 9.73 mi² North Branch Rock Creek near Norbeck basin (station 01647720) and the 1.01 mi² Manor Run near Norbeck basin (station 01647725) (fig. 1).

The investigation was designed to measure suspended-sediment loads leaving the impoundment and to collect the data necessary to estimate sediment inflow to the impoundment accurately.

The period of recorded data available at each of the streamflow and recording-precipitation gaging stations is given in table 1. Additional data were collected on the particle-size distribution of fluvial sediments, land use and land cover, and storm precipitation distribution.

Similar investigations of trap efficiency have been made in Colorado (Mundorff, 1968), Kentucky (Anttila, 1970), Ohio (Flint, 1972a), and West Virginia (Flint, 1972b). Sedimentation studies have also been made on Loch Raven and Prettyboy Reservoirs in Baltimore County, Md. (Holeman, 1965).

ACKNOWLEDGMENTS

This report was prepared by the U.S. Geological Survey in cooperation with the U.S. Soil Conservation Service. The author expresses his gratitude to the following: G. T. Munkittrick, State Conservationist, U.S. Soil Conservation Service; G. T. Stem, District Conservationist, U.S. Soil Conservation Service; and E.R.

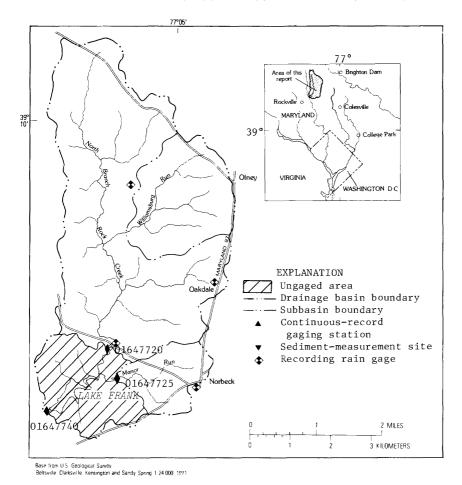


FIGURE 1.—Location of North Branch Rock Creek basin.

Keil, former State Conservationist, U.S. Soil Conservation Service for their encouragement and strong support during the project; and Ronald Dorsey, Maryland-National Capital Park and Planning Commission, for providing insight into the day-to-day operation of Lake Frank and data on flood levels in the impoundment.

BASIN CHARACTERISTICS AFFECTING SEDIMENT YIELDS

The four primary basin characteristics affecting sediment yields in the North Branch Rock Creek basin are climate, geology and soils, physiography and topography, and land use and land cover.

CLIMATE

The climate is rather humid and temperate, with a mean annual temperture of 13°C. Calculations based on the Environmental Data Service 1926-76 record of precipitation at nearby College Park, Md., indicate an average annual precipitation of 42.55 in. Average annual precipitation for water years 1968-76, for stations near the study area, ranges from 43.74 in. at Wheaton Regional Park to 47.02 in. at College Park. Precipitation averaged from four nearby rain gages ranged from 34.61 to 55.76 inches in 1968 and 1972, respectively. The driest month during the study was February 1968, precipitation 0.47 inch, and the wettest was June 1972, precipitation 14.11 inches. Herb and Yorke (1976) found no significant trends in the magnitude of rainstorms during 1968-74.

The long-term average monthly precipitation is highest in August, 4.89 in., and lowest in February, 2.77 in. During the 1968-76 water years, average monthly precipitation was at a minimum in January and at a maximum in June. The June maximum reflects the large amounts of rainfall associated with Hurricane Agnes in 1972. Figure 2 shows the average monthly precipitation at nearby stations during 1968-76. Summer precipitation is generally high-intensity rainfall associated with convective storms, and winter precipitation is generally rainfall from long-duration frontal storms.

Sediment yields are generally highest in the summer, when intense rainfall from convective storms provides sufficient energy for soil erosion. Herb and Yorke (1976) found that rainfall intensity was a statistically significant factor determining sediment yields in urban construction areas. They also found that the amount and intensity of storm runoff, which are closely correlated with the amount and intensity of rainfall, were also significant factors.

GEOLOGY AND SOILS

Soils of the eastern division of the Piedmont plateau are found in the study basin. These soils are developed in materials weathered from igneous and metamorphic rocks. The predominant soils are in the Manor-Chester-Glenelg association, which has a soft micaceous schist as parent material. The soils are primarily silt loams with a mixture of silty clay loams and channery silt loams. The silt loams and silty clay loams have about 30-percent sand or larger particles, and the channery silt loams have about 40-percent sand or larger particles. Most of the upland soils are in the Manor, Chester, Glenelg, Glenville, and Elioak series; and the stream valleys contain Worsham and Wehadkee silt loams.

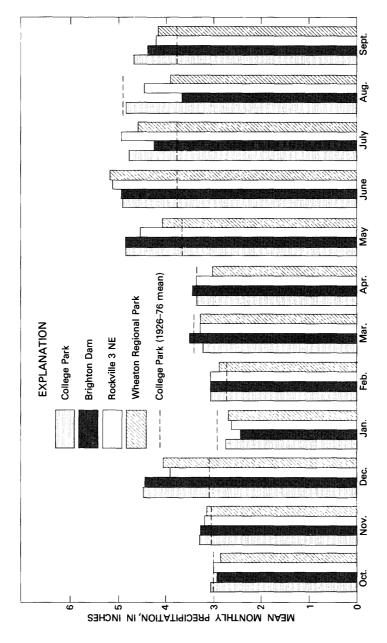


FIGURE 2.—Mean monthly precipitation at locations near the study area, October 1967 to September 1976.

The soils are generally uniform; however, the subsoils in the Manor and Glenville series have a weak structure, which makes them extremely susceptible to erosion when the surface soils are removed during construction (Yorke and Herb, 1978).

PHYSIOGRAPHY AND TOPOGRAPHY

The study area is in the eastern division of the Piedmont physiographic province. Altitudes in the North Branch Rock Creek basin range from about 570 ft in the headwaters of Williamsburg Run to about 270 ft at the North Branch Rock Creek near Rockville gaging station. Slopes of the stream valleys generally range from zero to 3 percent. Areas adjacent to the stream valleys generally have slopes greater than 8 percent and commonly in the 15- to 25-percent range. Slopes farther from the stream valleys are flatter and tend to range from zero to 8 percent near the drainage divides. Yorke and Herb (1978) present a detailed slope map of the North Branch Rock Creek basin and the adjacent Northwest Branch Anacostia River basin.

LAND USE AND LAND COVER

Owing to the fact that Lake Frank is in an urbanizing basin, land use and land cover changed almost continuously during the study period. Yorke and Herb (1978) determined that land use and land cover can be the major factor determining a basin's sediment yield in this area. Mansue and Anderson (1974) show similar results in New Jersey. As part of their study, Yorke and Herb obtained annual aerial photographs of the North Branch Rock Creek basin from 1966 through 1974. These aerial photographs were analyzed for land use and land cover by a dot-grid sampling procedure, and the land use and land cover in the basin was classified into 13 categories under the five general headings of farmland and parks, rural residential, urban residential, public and commercial, and construction. Acreage for each land use and land cover category is listed in table 2 for three subbasins and the total drainage basin of North Branch Rock Creek above the dam at Lake Frank. The three subbasins are North Branch Rock Creek near Norbeck, Manor Run near Norbeck, and the ungaged basin area. Land use and land cover for 1975 and 1976 was interpolated from the 1974 aerial photographs and data from a field inspection in March 1977. Because construction in 1975 and 1976 was minimal, these estimates are considered representative of actual land use and land cover during this period.

Figure 3 illustrates annual changes in three land use and land cover categories during 1968-76. Land use and land cover changes

TABLE 2.—Land use and land cover, in acres, in the North Branch Rock Creek basin, 1968-76

| | Fan | Farmland and parks | | | | residential | | resid | residential | comn | commercial | |
|----------|-------------|--------------------|-----------|-----------------|-------------|--|-----------------|-------|-----------------|-------|-----------------|-------------------|
| Č. | Crops Grass | 8 Forest | Water | Imper- vious | Grass | Forest | Imper- vious | Grass | Imper- vious | Grass | Imper- vious | Construc- tion |
| | | | North Bra | nch Rock (| reek near | North Branch Rock Creek near Norbeck (6,228 acres) | 3,228 acres | | | | | |
| 9681 | 389 206 | | 10 | 101 | 281 | 118 | 56 | 72 | 23 | 14 | 15 | 126 |
| | 1789 2037 | | 10 | 102 | 281 | 118 | 26 | 86 | 37 | 27 | 23 | 94 |
| : | | | 11 | 101 | 256 | 113 | 20 | 128 | 49 | 33 | 56 | 116 |
| 1971 18 | 1543 2105 | 5 1588 | 12 | 26 | 264 | 114 | 25 | 184 | 73 | 33 | 56 | 137 |
| : | | | 12 | 86 | 264 | 114 | 25 | 227 | 95 | 33 | 56 | 157 |
| : | | | 12 | 86 | 265 | 114 | 53 | 281 | 120 | 34 | 32 | 127 |
| : | | | 12 | 95 | 275 | 115 | 22 | 352 | 159 | 34 | 31 | 53 |
| : | | | 12 | 92 | 275 | 115 | 22 | 358 | 162 | 34 | 31 | 20 |
| 1976¹ 15 | 534 1992 | • | 12 | 95 | 275 | 115 | 55 | 364 | 165 | 34 | 31 | 11 |
| | | | | fanor Run | North North | Manor Run near Norheck (646 acres) | 100 | | | | | |
| | | | • | | | | | | | | | |
| 8961 | 12 205 | 200 | 0 | 13 | 28 | 30 | 15 | 19 | 5 | 9 | 7 | 92 |
| 6961 | | | 0 | 6 | 20 | 22 | 23 | 39 | 22 | 18 | 12 | 62 |
| 970 | | | 0 | 6 | 22 | 53 | 22 | 29 | 53 | 19 | 12 | 48 |
| 1971 | 22 122 | 171 | 0 | 6 | 28 | 53 | 22 | 68 | 31 | 19 | 12 | 35 |
| 972 | | | 0 | 6 | 28 | 53 | 22 | 102 | 35 | 19 | 12 | 22 |
| 973 | | | 0 | 6 | 28 | 53 | 22 | 113 | 40 | 19 | 12 | 5 |
| 1974 | | | 0 | 6 | 28 | 53 | 22 | 115 | 41 | 19 | 12 | 9 |
| 19751 | 22 115 | | 0 | 11 | 28 | 53 | 22 | 115 | 41 | 19 | 12 | 4 |
| 19201 | 99 115 | | • | 13 | χ, | 53 | 95 | 115 | 11 | 10 | 10 | 6 |

TABLE 2.—Land use and land cover, in acres, in the North Branch Rock Creek basin, 1968-76—Continued

| Crone | | | | | | Legiacina | | sa. | residential | COMP | commercial | |
|--------------------|-------|--------|------------|-----------------|------------|---|-----------------|--------|-----------------|-------|-----------------|-------------------|
| edoto. | Grass | Forest | Water | Imper- vious | Grass | Forest | Imper- vious | Grass | Imper- vious | Grass | Imper- vious | Construc- tion |
| | | | | Ungaged k | asin area | Ungaged basin area (1,141 acres) | a a | | | | | |
| 1968 140 | 428 | 284 | 53 | 6 | 0 | œ | 2 | 75 | 25 | က | | 113 |
| 1969 139 | 389 | 259 | 22 | 6 | 0 | 6 | 2 | 104 | 48 | 4 | က | 120 |
| 1970 136 | 340 | 258 | 22 | 14 | 0 | 4 | 2 | 171 | 65 | 22 | 9 | 89 |
| 1971 138 | 338 | 258 | 26 | 14 | 0 | 11 | 1 | 190 | 93 | 18 | 9 | 18 |
| 1972 139 | 322 | 258 | 99 | 15 | 0 | 7 | - | 204 | 103 | 17 | 9 | 13 |
| 1973 139 | 323 | 258 | 99 | 15 | 0 | 7 | - | 202 | 103 | 17 | 9 | 11 |
| 1974 139 | 320 | 258 | 59 | 16 | _ | 7 | _ | 204 | 103 | 17 | ro | 11 |
| 1975' 139 | 320 | 258 | 59 | 16 | - | 7 | _ | 506 | 104 | 17 | 5 | ∞ |
| $1976^1 \dots 139$ | 320 | 258 | 59 | 16 | | 7 | - | 208 | 106 | 17 | 2 | 4 |
| | | | | | | | | | | | | |
| | | | North Bran | ich Rock Cr | eek near B | North Branch Rock Creek near Rockville, Md. (8,015 acres) | d. (8,015 a | (cres) | | | | |
| 1968 1941 | 5696 | 2044 | 63 | 123 | 339 | 156 | 73 | 166 | 53 | 23 | 23 | 315 |
| : | 2578 | 1997 | 65 | 120 | 331 | 182 | 81 | 241 | 107 | 49 | 38 | 276 |
| 1970 1856 | 2539 | 2011 | 99 | 124 | 313 | 170 | 77 | 366 | 143 | 74 | 44 | 232 |
| : | 2565 | 2017 | 89 | 120 | 322 | 178 | 28 | 463 | 197 | 20 | 44 | 190 |
| | 2472 | 2001 | 89 | 122 | 322 | 174 | 28 | 533 | 233 | 69 | 44 | 195 |
| 1973 1703 | 2440 | 1981 | 89 | 122 | 323 | 174 | 79 | 299 | 263 | 20 | 20 | 143 |
| 1974 1695 | 2427 | 1974 | 71 | 120 | 334 | 175 | 81 | 671 | 303 | 20 | 48 | 46 |
| 19751 1695 | 2427 | 1974 | 71 | 122 | 334 | 175 | 81 | 629 | 307 | 20 | 48 | 35 |
| 10701 | 1 | | | | | | | 100 | | i | • | , |

'Land use and land cover estimated from 1974 aerial photos and field inspection in March 1977.

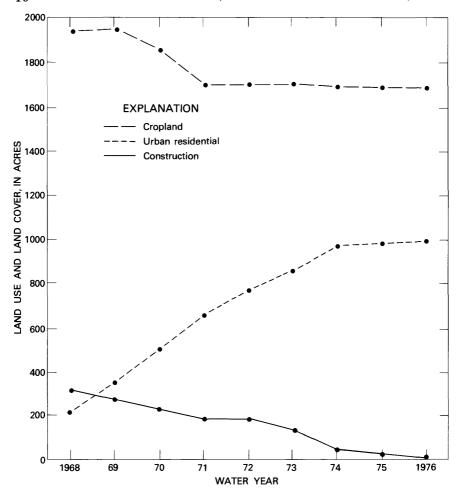


FIGURE 3.—Annual variations in basin land use and land cover, North Branch Rock Creek near Rockville, 1968-76.

during this period were characterized by a decline in cropland and construction area and a dramatic increase in the urban residential area. The percentage of construction in a basin can be a significant factor affecting storm-period suspended-sediment loads (Herb and Yorke, 1976). Even those urban areas without active construction sites provide a source of downstream sediment as stream channels adjust to accommodate an urbanized runoff regime (Yorke and Herb, 1978).

HYDRAULIC STRUCTURE

Lake Bernard Frank is impounded by a rolled-earth dam 576 ft wide and 78 ft high (fig. 4A). A grassed emergency spillway, 198 ft

wide, at the top-of-dam elevation (fig. 4B), brings the total width to 774 ft.

Normal releases of water from the impoundment are through a 24-in. x 30-in. orifice that has a crest elevation of 299.25 ft, in a concrete riser in the lake's pool (fig. 4C). A gate-operated 24-in. x 30-in. cold-water release orifice that has a crest elevation of 267.5 ft, and three 24-in.-diameter sluice gates at approximate elevations of 275, 282.5, and 291.5 ft are available for additional releases through the riser. The cold-water-release orifice and sluice gates are normally used only to lower the lake level for maintenance.

The principal spillway is a 42-in.-inside diameter reinforced concrete conduit, which extends $460 \, \text{ft}$ from the base of the concrete riser to an impact basin (fig. 4D) at the downstream face of the dam.

The impoundment is oriented northeast-southwest and is rather sinous, as determined by the area's topography. The permanent pool is 5,700 ft long, and the maximum design high-water pool is 9,400 ft. The impoundment has a design sediment-pool area of 35 acres and a sediment-pool capacity of 261 acre-ft. The permanent-pool area is 56 acres and has a capacity of 780 acre-ft. Floodwater detention at the crest of the emergency spillway is 3,894 acre-ft, for a total capacity of 4,576 acre-ft. Altitude-capacity and altitude-surface area relations for Lake Frank are presented in table 3.

STREAMFLOW

Daily streamflow data were collected at three sites (fig. 1) by standard stream-gaging procedures described by Carter and Davidian (1968). Data were gathered at station 01647740 (fig. 5) immediately downstream from Lake Frank from August 1967 through September 1977. Daily streamflow data were collected at stations 01647720 (fig. 5) and 01647725 (fig. 7) from October 1966 through September 1974, except during October and November 1966, when no data were collected at 01647725.

If the severe storms of June 1972 and September 1975 are excluded, the mean monthly discharge is highest from February to April and lowest in September or October. This distribution of runoff is almost exactly opposite the distribution of precipitation. The difference is probably caused by the differences in potential evapotranspiration between early spring and early fall. If the two large storms are included, mean monthly runoff is lowest in October and highest in June.

Average annual discharge at North Branch Rock Creek near Rockville ranged from 3,152 to 11,886 ft³/s-d (table 4) and includes the effect of the drought at the beginning of the study and the wetter years near the end of the study.

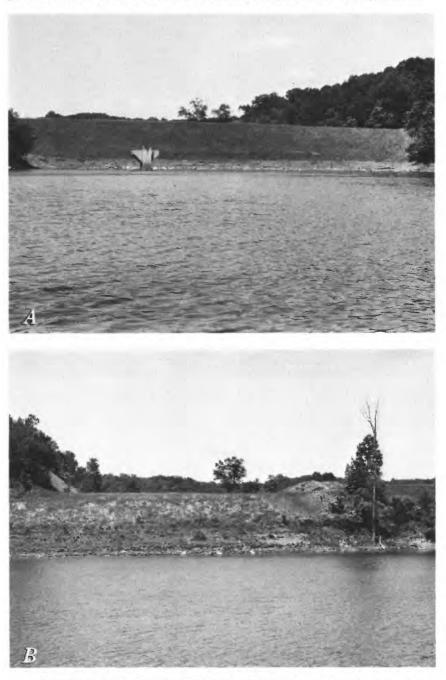
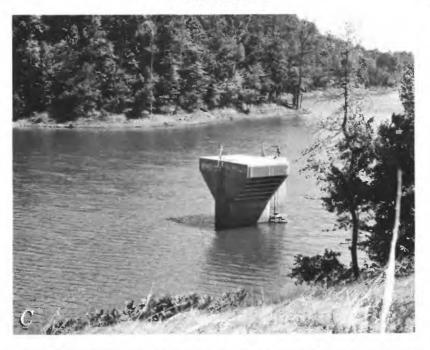


Figure 4.—Lake Bernard Frank (A) earth-fill dam (view from upstream), left bank), and (D) concrete impact





(B) emergency spillway (view from upstream), (C) concrete riser (view from basin (view from downstream).

14 SEDIMENT-TRAP EFFICIENCY, NORTH BRANCH ROCK CREEK, MD.

Table 3.—Altitude, capacity, and surface-area relationships of Lake Bernard Frank (as designed)

[Modified from data furnished by Soil Conservation Service]

| Altitude (feet above NGVD of 1929) ³ | Approximate capacity (acre-ft) | Approximate surface area (acres) | Altitude (feet above NGVD of 1929) ³ | Approximate capacity (acre-ft) | Approximate surface area (acres) |
|--|--------------------------------|---|--|--------------------------------------|---|
| 268 | 0 | 0.0 | 308 | 1,450 | 75.0 |
| 270 | 0.7 | .7 | 310 | 1,598 | 79.0 |
| 272 | 5.5 | 2.4 | 312 | 1,750 | 84.0 |
| 274 | 10 | 4.1 | 314 | 1,937 | 89.0 |
| 276 | 26 | 6.8 | 316 | 2,110 | 95.0 |
| 278 | 50 | 12.0 | 318 | 2,320 | 102.0 |
| 280 | 81 | 19.5 | 320 | 2,536 | 110.0 |
| 282 | 123 | 25.5 | 322 | 2,750 | 118.0 |
| 284 | 180 | 30.5 | 324 | 3,014 | 129.0 |
| 286 | 245 | 34.5 | 326 | 3,250 | 140.0 |
| 288 | 320 | 39.0 | 328 | 3,500 | 150.0 |
| 290 | 399 | 43.0 | 330 | 3,883 | 163.0 |
| 292 | 480 | 46.0 | 332 | 4,200 | 175.0 |
| 294 | 581 | 49.5 | 3342 | 4,576 | 187.0 |
| 296 | 680 | 53.0 | 336 | 4,900 | 199.0 |
| 2981 | 780 | 56.0 | 338 | 5,300 | 214.0 |
| 300 | 904 | 60.0 | 340 | 5,812 | 225.0 |
| 302 | 1,020 | 63.0 | 342 | 6,300 | 240.0 |
| 304 | 1,157 | 67.0 | 344 | 6,772 | 255.0 |
| 306 | 1,300 | 71.0 | | | |

^{&#}x27;Normal pool.

²Crest of emergency spillway.

³National geodetic vertical datum of 1929.



FIGURE 5.—Gaging station (arrow), North Branch Rock Creek near Rockville (view looking downstream from top of dam).



FIGURE 6.—Gaging station, North Branch Rock Creek near Norbeck (view from upstream).



FIGURE 7.—Gaging station, Manor Run near Norbeck (view from upstream).

Table 4.—Annual discharges, in cubic feet per second-days, for gages in the North Branch Rock Creek basin, 1968-76

| | | Gaging Statio | ons |
|---------------|--|------------------------------|--|
| Water year | North Branch Rock Creek near Norbeck | Manor Run near Norbeck | North Branch Rock Creek near Rockville |
| 1968 | | 361 | 3,378 |
| 1969 | | 315 | 3,152 |
| 970 | | 399 | 4,954 |
| 1971 | 5,018 | 571 | 6,967 |
| 972 | 8,508 | 844 | 11,886 |
| 973 | 6,320 | 733 | 8,160 |
| .974 | 3,650 | 397 | 4,492 |
| .975 | 5,646 | 1618 | 7,570 |
| 976 | 4.294 | 1431 | 5,382 |

¹Estimated by correlation with North Branch Rock Creek near Norbeck.

SEDIMENT METHODOLOGY

The sediment load of a stream consists of suspended-sediment load and bedload. Suspended load is defined as that part of the load transported while distributed throughout the flowing water by upward components of turbulence or colloidal forces. Bedload consists of sediment that moves by sliding, rolling, or skipping along the steambed; it generally remains in contact with the bed. Standard sediment-sampling equipment samples only that part of the suspended-sediment load in transport more than 0.3 ft above the bed. No direct bedload measurements were attempted.

Concurrent daily streamflow records are available for North Branch Rock Creek near Norbeck and at the outlet of Lake Frank for the 1968-76 water years. Daily streamflow records are available for Manor Run for the 1968-74 water years. The two upstream gages measure inflow to Lake Frank from 86 percent of the contributing drainage area. The mean discharge at the North Branch Rock Creek near Rockville gage was 17.0 ft³/s, or 12,300 acre-ft per year during 1968-76. Disregarding losses to evaporation and leakage and gains from precipitation on the lake, the mean annual outflow is assumed to be equivalent to the total mean annual inflow to Lake Frank during 1968-76.

Storm-period suspended-sediment loads were determined by collecting samples manually or automatically during storm runoff, determining the concentration in a laboratory, and computing sediment loads by the subdivided-day method (Guy and Norman, 1970; Guy, 1973; Porterfield, 1972).

Peak suspended-sediment concentrations generally preceded peak water discharges of North Branch Rock Creek near Norbeck. The same pattern was observed on Manor Run for most storms, but there was a slight tendency toward simultaneous concentration and discharge peaks. Anttila and Tobin (1978) believe that advanced concentration peaks reflect a basinwide abundance of sediment readily available for transport. The continuous construction activity in the North Branch Rock Creek basin would provide such a ready source of new sediment.

SEDIMENT INFLOW

SUSPENDED SEDIMENT

Storm-period suspended-sediment loads were determined at the two gaging stations upstream from Lake Frank. Suspended-sediment samples were collected at the Manor Run station with single-stage samplers located at preset flow elevations. These samplers can obtain samples only when the stream stage is rising. The single-stage samples were supplemented with numerous depth-integrated cross-section samples taken by hand to define suspended-sediment concentrations on both rising and falling stages. Single-stage samplers were used at North Branch Rock Creek near Norbeck, but the primary sampling was done by an automatic pumping suspended-sediment sampler, which sampled at preset elevations on rising and falling stages. Depth-integrated cross-section samples were also taken by hand at this site to verify the automatic samplers.

Daily suspended-sediment loads for unmeasured storm days during the partial-record and post-data collection periods were estimated from records of daily discharge and daily suspended-sediment transport curves. A suspended-sediment transport curve relates daily streamflow to daily suspended-sediment load. A series of transport curves was used from 1968 through 1976 because the streamflow-sediment transport relations changed as land use and land cover within the basin changed (Yorke and Herb, 1978). Figures 8 and 9 show suspended-sediment transport curves for North Branch Rock Creek and Manor Run.

Five suspended-sediment transport curves were developed for Manor Run and seven for North Branch Rock Creek near Norbeck. Each curve applies to a period during which land use and land cover was relatively constant. The transport curves were based on data collected during storm runoff that had adequate streamflow and sediment load definition.

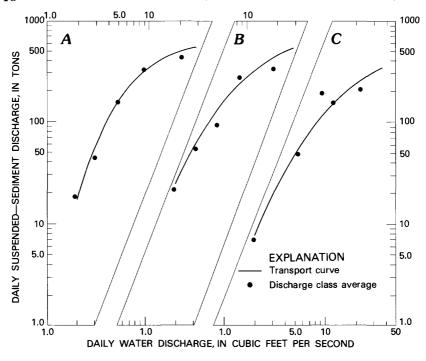
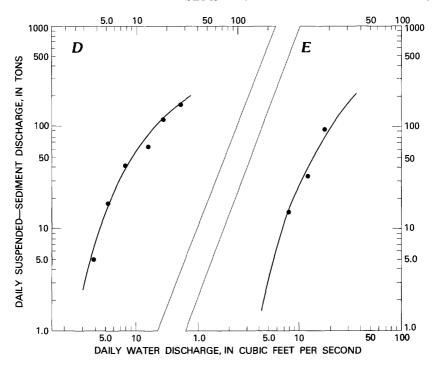


FIGURE 8.—Suspended-sediment transport curves (A) Oct. 1967-Sept. 1968, (B) 1973-Sept. 1976; Manor

Daily streamflow and sediment-load data collected during the 1973-74 water years were used to develop transport curves for the 1975-76 water years for Manor Run but not for North Branch Rock Creek near Norbeck. There were major changes in land use and cover, primarily due to construction, between the 1973-74 and 1975-76 periods in North Branch Rock Creek basin, but only minimal changes between the two periods in Manor Run basin. Accordingly, streamflow and sediment-load data collected in the 1975 water year were used to develop the 1975-76 transport curve for North Branch Rock Creek.

Owing to the fact that the transport curves were based on storm-day data, suspended-sediment loads were estimated only for storm-runoff days. Storm runoff occurred on 14 percent of the days in Manor Run and North Branch Rock Creek near Norbeck during 1968-76. Yorke and Herb (1978) found that in the adjacent Anacostia River basin, 94 percent of the suspended-sediment load was transported during high runoff. This high runoff occurred during fewer than 6 percent of the days. Therefore, suspended-sediment loads measured or estimated for storm-runoff during 14 percent of the days probably account for at least 95 percent of the

19



Oct. 1968-Mar. 1970, (C) Apr. 1970-Dec. 1970, (D) Jan. 1971-Mar. 1973, (E) Apr. Run near Norbeck.

total suspended-sediment load, and are assumed to be representative of the total suspended load.

Days defined as having storm runoff were determined by examining daily streamflow records and choosing those days during which the previous day's discharge was at least doubled. The storm period was considered to continue until the recession in water discharge became fairly constant. This procedure usually resulted in storm periods of 1 or 2 days. As most of the suspended sediment in this area is transported on the rising stage, as indicated by concentration peaks preceding water discharge peaks, total storm suspended-sediment loads should be adequately estimated by this procedure.

Although the daily discharge and sediment-transport curve technique provides adequate estimates of suspended-sediment loads when daily streamflow is known, a modified technique was needed for Manor Run for 1975-76, when no daily discharges were available. The modified technique required estimates of daily discharges for Manor Run followed by the daily discharge and sediment-transport procedures discussed earlier.

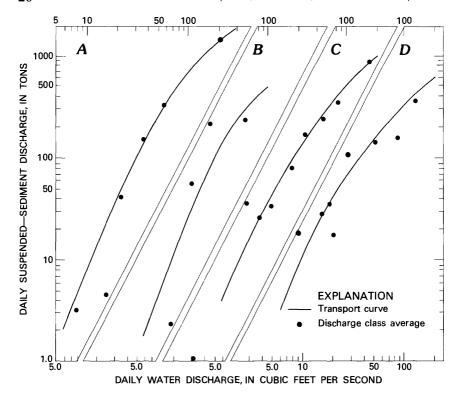


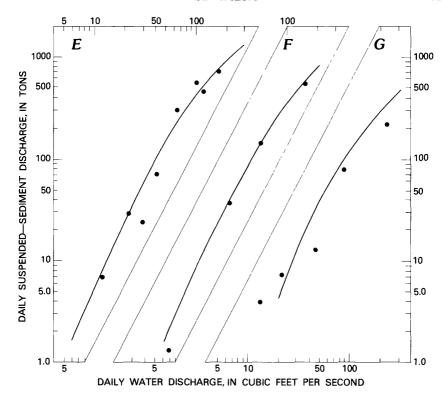
Figure 9.—Suspended-sediment transport curves (A) Oct. 1967-Mar. 1968, (B) Apr. Dec. 1973, (F) Jan. 1974-Sept. 1974, (G) Oct. 1974-

A regression equation using concurrent daily discharges at North Branch Rock Creek near Norbeck was used to estimate discharges for Manor Run. Discharges on the 1st, 6th, 11th, 16th, 21st, and 26th of each month during the 1973 and 1974 water years, or 144 sets of data, were used to develop the equation. This pseudorandom procedure should provide a data set with no bias toward days with low or high discharges.

An initial, graphical solution indicated that the relation between concurrent daily discharges for Manor Run and North Branch Rock Creek near Norbeck could be described by two straight lines. One line, based on 57 data points, defined the relationship for North Branch Rock Creek daily discharges less than 7.0 ft³/s. A second line, based on 87 data pairs, defined the relationship for North Branch Rock Creek daily discharges equal to or greater than 7.0 ft³/s.

The linear regression model used in the analysis was of the form:

$$\log M = b_0 + b_1(\log N)$$



1968-Mar. 1969, (C) Apr. 1969-Mar. 1971, (D) Apr. 1971-Dec. 1971, (E) Jan. 1972-Sept. 1976; North Branch Rock Creek near Norbeck.

where

log *M* = logarithm (base 10) of Manor Run daily discharge, in cubic feet per second;

log N = logarithm (base 10) of North Branch Rock Creek nearNorbeck daily discharge, in cubic feet per second;

 b_0 = regression constant; and

 b_1 = regression coefficient.

It was found that the logarithmic (base 10) transformation was useful to achieve homoscedasticity, or equal variance about the regression line. The linear regression analysis developed the following equations:

$$\log M = -0.74 + 0.65 (\log N) \tag{1}$$

$$\log M = -1.13 + 1.09 \; (\log N) \tag{2}$$

Equation 1 applies when the average daily discharge at North

Branch Rock Creek near Norbeck was less than $7.0 \, \text{ft}^3/\text{s}$, and equation 2 applies when the daily discharge was equal to or greater than $7.0 \, \text{ft}^3/\text{s}$.

The validity of the regression equations was tested by estimating daily discharges for Manor Run using daily discharges at North Branch Rock Creek for the 1972 water year. The estimated discharges were then compared with those measured on Manor Run. As no 1972 data were used in the regression model calibration, the 1972 synthetic discharges for Manor Run are considered to be an unbiased estimate of an independent data set. Table 5 shows the monthly and yearly totals of the synthetic and measured daily discharges for Manor Run.

Although table 5 indicates that estimates of monthly discharges depart widely from measured monthly discharges, the annual estimate is closer to the measured, due to the compensating nature of the monthly departures. If the month of June, containing data from Hurricane Agnes, is eliminated, the estimated 11-month discharge is 595.1 ft³/s-d as compared with a measured 11-month total discharge of 608.5 ft³/s-d. June can be dropped from the comparison because the maximum daily discharge during Hurricane Agnes was more than 15 times greater than the maximum daily discharge used to calibrate the regression model.

As only storm days were used to estimate annual sediment inflows, the relation between estimated and measured discharge was tested on 57 storm days in the 1972 water year. All storm-day discharges were estimated using equation 2 which is applicable for all North Branch Rock Creek daily discharges above 50 percent duration. If the runoff associated with Hurricane Agnes is excluded, the regression equation underestimates the 1972 storm-day discharges by about 15 percent. An error of this magnitude would probably not cause a significant underestimate of the total sediment load. None of the daily discharges of the North Branch Rock Creek near Norbeck in the 1975 and 1976 water years greatly exceeded the range of data used in the regression model calibration, so the estimates of daily discharge for Manor Run are acceptable.

Daily storm suspended-sediment loads for the 1975-76 water years were estimated from the sediment-transport curve by applying the daily water discharges determined from equation 2. Although the daily and monthly estimates may be in error, the yearly totals shown in table 6 are relatively accurate.

Table 5.—Estimated monthly discharge totals for 1972 water year compared to measured monthly discharges for Manor Run near Norbeck

| Monthly (ft ³ / | _ | Percentage |
|----------------------------|----------|------------|
| Estimated | Measured | error |
| 1971: | | |
| October | 63.2 | - 1 |
| November 64.4 | 67.0 | - 4 |
| December | 31.3 | +12 |
| 1972: | | |
| January 40.0 | 36.1 | ×11 |
| February 108 | 81.1 | -25 |
| March 57.0 | 55.2 | + 3 |
| April 73.1 | 68.3 | + 7 |
| May 80.6 | 59.3 | +36 |
| June346 | 235 | +47 |
| July 68.9 | 83.1 | -17 |
| August 19.9 | 25.6 | -22 |
| September 12.2 | 11.4 | + 7 |
| Total 941.1 | 843.5 | +12 |

Table 6.—Annual storm suspended-sediment inflows! to Lake Bernard Frank from Manor Run and North Branch Rock Creek

| Water year | Storm suspended-s | ediment inflow, in tons per yea |
|---------------|-------------------|---------------------------------|
| year | Manor Run | North Branch Rock Creek |
| 1968 | 4,209 | 3,113 |
| 1969 | 3,454 | 4,504 |
| 1970 | 3,508 | 7,302 |
| 1971 | | 9,465 |
| 1972 | | 14,867 |
| 1973 | | 11,062 |
| 1974 | 512 | 4,354 |
| 1975 | 806 | 3,986 |
| 1976 | 587 | 1,830 |

¹Measured and estimated.

BEDLOAD

Bedload was not measured directly, but was estimated by empirical equations, as described by Yorke and Herb (1978). Thus, the Meyer-Peter and Muller equation (Sheppard, 1960) and the Schoklitsch equation (Shulits, 1935) were used to compute the bedload. A bed material sample from the channel (fig. 10) and discharge measurements from 19 to 338 ft³/s for North Branch Rock Creek near Norbeck were used in the computations. Bedload-transport curves determined from the Schoklitsch and Meyer-Peter and Muller formulas were then used with a flow-duration curve to compute average annual bedload transport for North Branch Rock Creek near Norbeck.

Average annual bedloads for 1968-76 of 1,370 tons and 1,290 tons were computed from the Meyer-Peter and Muller and the Schoklitsch equations, respectively. These computed bedloads accounted for 13.7 and 16.1 percent of the total average annual sediment yield for the same period. Yorke and Herb (1978) computed bedloads of 6 and 13 percent for the adjacent Northwest Branch Anacostia River basin. These four estimates of bedload were averaged, giving double weight to the North Branch Rock Creek data, to obtain a bedload contribution of 13 percent of the total load. The 13 percent value was assumed to be applicable to both North Branch Rock Creek and Manor Run. The bedload contribution was combined with the suspended-sediment load estimate for the upstream stations to estimate yearly total sediment inflow to Lake Frank. Bedload from the ungaged area was assumed minimal because most of the area is adjacent to the impoundment and lacks well-defined stream channels.

UNGAGED SEDIMENT YIELD

The gaging stations on Manor Run and North Branch Rock Creek near Norbeck monitored flow and sediment from only 10.74 mi² of the 12.5 mi² drainage area above station 01647740. Therefore, the sediment contribution of the ungaged 14 percent of the basin was estimated to determine trap efficiency.

Yorke and Herb (1978) estimated average annual sediment yields under different land use and land cover conditions in the Northwest Branch Anacostia River and North Branch Rock Creek basins (table 7).

The land use and land cover categories given in table 6 are generally the same as those in table 2. However, impervious area in the farmland category was assigned to the crop category because most of the impervious area consists of dirt roads and unimproved



Figure 10.—Channel of North Branch Rock Creek near Norbeck in vicinity of bedmaterial sampling point (view from upstream).

Table 7.—Annual suspended-sediment yields for land use and land cover categories for Northwest Branch Anacostia River and North Branch Rock Creek basins (Yorke and Herb, 1978)

| Land use and land cover An category | nual sediment yield (tons/acre) |
|-------------------------------------|------------------------------------|
| Forest | 0.03 |
| Grass | ,2 |
| Crops | 2.7 |
| Rural residential | 5 |
| Urban residential | 3.75 |
| Public and commercial | |
| Construction ¹ | |

¹Construction-area weighted average yield computed using ungaged subbasin construction area and four sediment yields for the Manor Run basin (Yorke and Herb, 1978).

roadside ditches (Yorke and Herb, 1978). In addition to the sediment yields shown in table 7, the obvious yearly sediment yield of 0 tons per acre per year was used for lake and pond areas.

When the acres in each category of land use and land cover are multiplied by the appropriate annual sediment yield, the annual sediment yields shown in table 8 are obtained.

TABLE 8.—Annual suspended-sediment yields, in tons, for land use and land cover categories, and total annual sediment yields, in tons, for ungaged portion of North Branch Rock basin, 1968-76

| Water | | | J | Land use and land cover categories | over categories | | | | |
|-------|--------|-------|-------|------------------------------------|----------------------|--------------------------|--------------|-------|----------|
| year | Forest | Grass | Crops | Rural | Urban residential | Public and commercial | Construction | Water | Total |
| 1968 | 8.52 | 85.6 | 402.3 | 5.0 | 375.0 | 1.2 | 9638.9 | 0 | 10516.52 |
| 1969 | 7.77 | 77.8 | 399.6 | 5.5 | 570.0 | 2.1 | 10236.0 | 0 | 11298.77 |
| 0761 | 7.74 | 68.0 | 394.2 | 3.0 | 885.0 | 9.6 | 5800.4 | 0 | 7167.94 |
| 1971 | 7.74 | 9.79 | 402.3 | 0.9 | 1061.3 | 8.1 | 1535.4 | 0 | 3088.44 |
| 1972 | 7.74 | 64.4 | 405.0 | 4.0 | 1151.3 | 8.1 | 1108.9 | 0 | 2749.44 |
| 1973 | 7.74 | 64.6 | 405.0 | 4.0 | 1155.0 | 8.1 | 938.3 | 0 | 2582.74 |
| 1974 | 7.74 | 64.0 | 405.0 | 4.5 | 1151.3 | 8.1 | 938.3 | 0 | 2578.94 |
| 1975 | 7.74 | 64.0 | 405.0 | 4.5 | 1162.5 | 8.1 | 682.4 | 0 | 2334.24 |
| 1976 | 7.74 | 64.0 | 405.0 | 4.5 | 1177.5 | 8.1 | 341.2 | 0 | 2008.04 |

SEDIMENT OUTFLOW

Daily suspended-sediment loads were determined at station 01647740, immediately downstream from Lake Frank (fig. 1). An automatic pumping suspended-sediment sampler took one or more daily samples. The intake orifice for the sampler was mounted on a concrete pier (fig. 11) on the left bank of the outflow channel. The daily automatic samples were supplemented with depth-integrated samples collected by hand on routine visits to the gaging station and during storm runoff. Bedload outflow from Lake Frank was considered to be negligible because the bulk of the material passing through the impoundment is sufficiently fine to be in suspension at the downstream gaging station.

EFFECTS OF IMPOUNDMENT STORM RUNOFF AND SEDIMENT DISCHARGE

Flood frequency analyses for Manor Run near Norbeck (Yorke and Herb, 1978), 1967-74, show peak discharges of 310, 590, and 990 ft³/s at exceedance probabilities of 50, 20, and 10 percent, respectively. A flood having an exceedance probability of 50 percent has a 50 percent chance of being exceeded in any given year; other exceedance probabilities are similarly defined. Flood frequency analyses for North Branch Rock Creek near Norbeck, 1967-77, indicate peak discharges of 910; 2,120; and 3,510 ft³/s at exceedance probabilities of 50, 20, and 10 percent, respectively. Below Lake Frank, the average annual maximum peak for the 1968-76 water years was approximately 150 ft³/s, and a maximum peak of 420 ft³/s occurred in 1972.

Examination of upstream and downstream flood peaks on North Branch Rock Creek and Manor Run show that the Lake Frank



FIGURE 11.—Channel of North Branch Rock Creek near Rockville. Intake for automatic pumping suspended-sediment sampler is located on concrete pier (arrow) (view from downstream).

impoundment reduces downstream flood peaks. During May 13-14, 1971, the basin received 2.15 in. of rainfall. This precipitation was evenly distributed across the basin, but the maximum 15-minute intensity was 1.98 in./h (inches per hour) in the Manor Run basin and 1.32 in./h in the North Branch Rock Creek basin near Norbeck. Runoff hydrographs, shown in figure 12 for the upstream and downstream stations, clearly show the effects of the impoundment. The peak discharges, expressed as (ft³/s)/mi², of Manor Run and North Branch Rock Creek near Norbeck were 207 and 51.2, respectively. The exceedance probability of such peaks is 95 to 99 percent. Below Lake Frank the peak was measured at 7.0 (ft³/s)/mi² during the same runoff.

Another example of the attenuating effect of Lake Frank was observed during Hurricane Agnes. On June 21–22, 1972, 11.25 in. of precipitation from Hurricane Agnes was measured at nearby Wheaton Regional Park (Bailey and others, 1975). Peak discharges of Manor Run and North Branch Rock Creek near Norbeck were 900 (ft³/s)/mi² and 1,040 (ft³/s)/mi². Below Lake Frank, the peak discharge was 33.6 (ft³/s)/mi². The maximum elevation of the water surface reached in the lake during the runoff after Hurricane Agnes was 329 ft (Ronald Dorsey, oral commun., 1978). This is equivalent to 2,850 acre-ft of flood storage.

Lake Frank not only exerts a major effect on flood peaks, but it also significantly affects suspended-sediment loads during storm runoff. Figure 13 is a plot of instantaneous suspended-sediment loads at the three gaging stations in the study area for May 13–14, 1971. Precipitation and streamflow data during this storm are given in the section on streamflow.

Peak instantaneous suspended-sediment loads at the upstream stations were 15,000 tons/d and 4,880 tons/d for Manor Run and North Branch Rock Creek, respectively. During the same two-day event, the maximum instantaneous suspended-sediment load downstream from Lake Frank was 33 tons/d. The total suspended-sediment load measured at Manor Run and North Branch Rock Creek near Norbeck was 991 tons on May 13 and 14; whereas the total measured load below the lake was 31 tons.

During the June 21-23, 1972, period of Hurricane Agnes, a suspended-sediment load of 3,270 tons was measured at North Branch Rock Creek near Norbeck. Downstream from the impoundment, 593 tons of suspended sediment were measured over the same period, and another 332 tons of suspended sediment were measured over the 5 succeeding days.

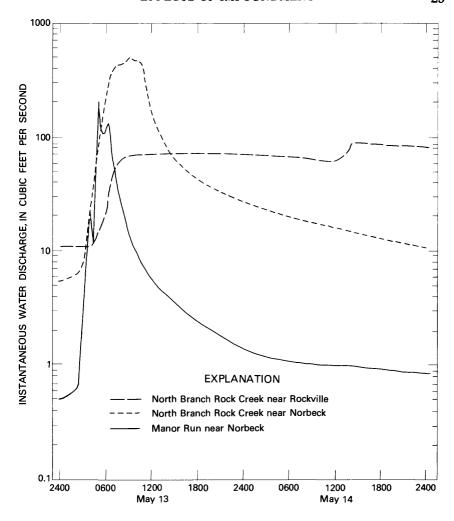


FIGURE 12.—Hydrograph for three locations in the North Branch Rock Creek basin, storm of May 13-14, 1971.

PARTICLE SIZE

Table 9 summarizes the results of particle-size analyses of suspended-sediment samples taken at the three sediment-monitoring stations in the North Branch Rock Creek basin. Sediment discharge-weighted percentages of sand-sized particles were 13 and 19 at the upstream stations and zero at the station below the impoundment. Silt percentages were 45 and 54 upstream

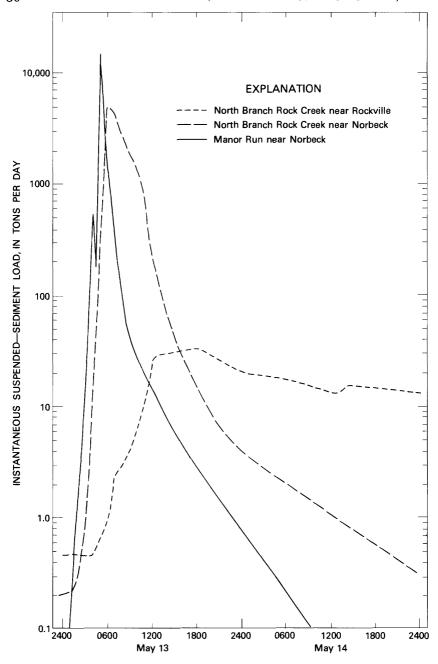


FIGURE 13.—Instantaneous suspended-sediment load for storm of May 13-14, 1971.

Table 9.—Particle-size distribution of suspended sediment in the North Branch Rock Creek basin

| Date | Water discharge (ft ³ /s) | Suspended- sediment concentra- tion | Suspended- sediment discharge | | nt susp nt in si | ended ze class |
|---------------------|--|--|---------------------------------------|------|---------------------|-------------------|
| | (11-78) | (mg/L) | (tons/d) | Sand | Silt | Clay |
| North Branch I | Rock Creel | near Norbe | k, Md. 1969- | 75 | | |
| June 18, 1969 | 90 | 4,090 | 994 | 5 | 58 | 37 |
| Apr. 2, 1970 | 143 | 2,840 | 1,100 | 12 | 56 | 32 |
| Feb. 2, 1973 | 342 | 2,400 | $2,2\bar{20}$ | 13 | 54 | 33 |
| Apr. 4, 1973 | 380 | 1,460 | 1,500 | 23 | 46 | 31 |
| June 2, 1974 | 151 | 344 | 140 | 3 | 50 | 47 |
| Sept. 24, 1975 | 194 | 464 | 243 | 4 | 62 | 34 |
| Sediment discharge- | | | | | | |
| weighted average | _ | _ | _ | 13 | 54 | 33 |
| Manor | Run near N | Vorbeck, Md. | 1967-70 | | | |
| May 7, 1967 | 53 | 10,000 | 1,430 | 23 | 46 | 31 |
| June 22, 1967 | 18 | 28,400 | 1,380 | 8 | 50 | 42 |
| Mar. 18, 1968 | 6.3 | 2,780 | 47 | 4 | 48 | 48 |
| June 19, 1968 | 97 | 9,890 | 2,590 | 25 | 39 | 36 |
| July 22, 1969 | 30 | 22,500 | 1,822 | 12 | 52 | 36 |
| July 22, 1969 | 2.6 | 2,610 | 18 | 1 | 41 | 58 |
| Sept. 10, 1970 | 77 | 6,380 | 1,330 | 25 | 43 | 32 |
| Sediment discharge- | | | | | | |
| weighted average | _ | _ | _ | 19 | 45 | 36 |
| North Branch R | ock Creek | near Rockvi | lle, Md. 1972-7 | 76 | | |
| June 1, 1972 | 44 | 213 | 25 | 0 | 7 | 93 |
| June 22, 1972 | 404 | 415 | 453 | 0 | 17 | 83 |
| Jan. 28, 1976 | | 46 | 3.5 | 2 | 18 | 80 |
| Sediment discharge- | | | · · · · · · · · · · · · · · · · · · · | | | |
| weighted average | - | _ | - | 0 | 16 | 84 |

and 16 downstream. Below Lake Frank, 84 percent of the suspended-sediment load was clay size, while upstream the percentages were 33 and 36.

A relation exists between the percentages of sand, silt, and clay transported as suspended sediment, and water discharge of North Branch Rock Creek near Norbeck. The sand percentage is proportional to the logarithm of water discharge, while the silt and clay percentages are inversely proportional to the logarithm of

water discharge as shown in figure 14. These relations can be explained by the fact that the stream becomes more competent to transport larger particles at higher discharges, while the amount of finer material in transport remains a relatively constant function of availability. Although the relation between the percentage of suspended sediment in a size class and the logarithm of water discharge seems to be linear on North Branch Rock Creek, this is not true in Manor Run (fig. 15). The distribution of data in figure 15 indicates a nonlinear relation; although additional data could produce a linear relation similar to that of North Branch Rock Creek near Norbeck.

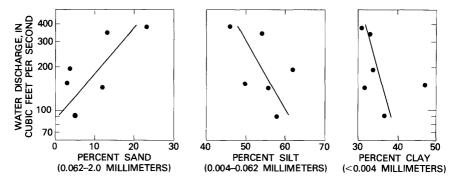


FIGURE 14.—Relation of sand, silt, and clay content of suspended sediment to water discharge, North Branch Rock Creek near Norbeck, 1969-75.

TRAP EFFICIENCY

Table 10 summarizes the estimated and measured sediment loads entering Lake Frank and the measured loads leaving Lake Frank, 1968-76. Figures 16 and 17 present the same data graphically and show that sediment inflow greatly exceeded sediment outflow.

Estimated annual sediment contributions to Lake Frank from all sources ranged from 0.57 to 2.83 tons/acre during 1968-76 (table 11). Maximum yield occurred during 1969-72 and averaged 2.48 tons/acre. The annual yield in tons per acre per inch of runoff decreases consistently (fig. 18) from a high of 0.272 in 1969 to 0.037 in 1976. Yorke and Herb (1978) attribute much of this decrease to the decline in construction area within the basin, as shown in figure 3, and an increase in the use of on site sediment controls in urban construction areas.

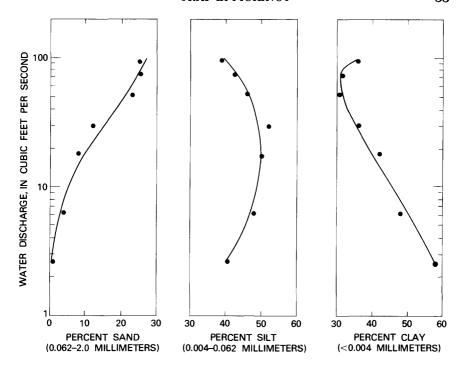


FIGURE 15.—Relation of sand, silt, and clay content of suspended sediment to water discharge, Manor Run near Norbeck, 1967-72.

The trap efficiency of an impoundment is the ratio of the amount of sediment trapped to the total amount of sediment entering. Trap efficiency can be computed by the formulas:

$$TE = 100 \frac{A}{A+B} \tag{3}$$

$$TE = 100 \frac{C - B}{C} \tag{4}$$

where

TE = trap efficiency of the impoundment, in percent;

A = weight of sediment deposited in impoundment, in tons;

B = weight of sediment discharged from the impoundment, in tons; and

C = weight of sediment entering the impoundment, in tons.

Table 10.—Annual sediment inflow and outflow, in tons, Lake Bernard Frank, 1968-76

| Manor Run Water Suspended sedioad year sediment 1968 .4,209 629 1969 .3,454 516 1970 .3,508 524 1971 .2,352 351 | North Branch Rock Creek Suspended Bedlos sediment 9 3,113 466 | Rock Creek Bedload 465 | Ungaged Total load | Total Load | |
|---|---|------------------------|--------------------------|---------------------|-----------------------|
| Suspended sediment 4,209 3,454 3,508 2,352 | | Bedload 465 | Total load | | |
| 3,454 3,454 3,508 3,508 | | 465 | | from all sources | Suspended sediment |
| 3,454 | | | 10,517 | 18,933 | 511 |
| 3,508 | | 673 | 11,299 | 20,446 | 226 |
| 2,352 | | 1,090 | 7,168 | 19,592 | 504 |
| 0070 | | 1,410 | 3,088 | 16,666 | 979 |
| 904,7 | • | 2,220 | 2,749 | 22,604 | 1,820 |
| 1,702 | _ | 1,650 | 2,583 | 17,251 | 720 |
| 512 | | 651 | 2,579 | 8,172 | 258 |
| 908 | | 296 | 2,334 | 7,842 | 569 |
| 1976 587 88 | | 273 | 2,008 | 4,786 | 320 |
| Total 19,538 2,918 | 8 60,483 | 9,028 | 44,325 | 136,292 | 5,905 |

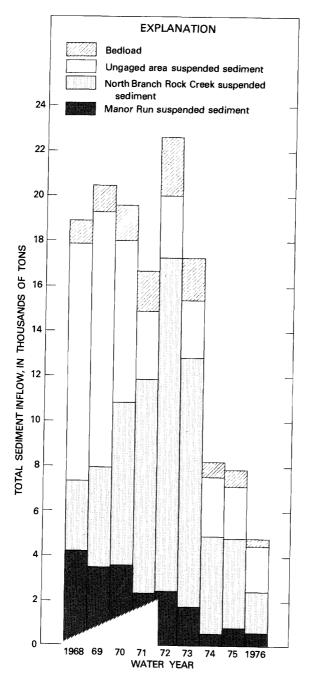


FIGURE 16.—Annual sediment inflow, Lake Bernard Frank, by water year.

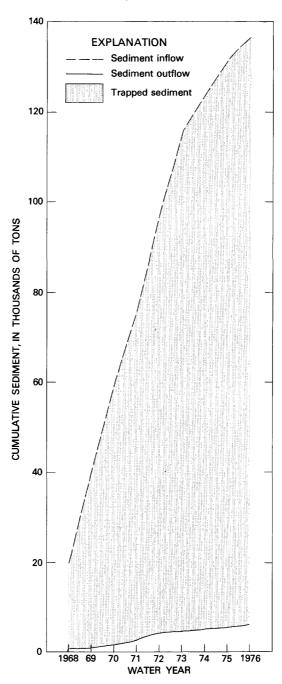


FIGURE 17.—Cumulative sediment inflow and outflow, Lake Bernard Frank, by water year.

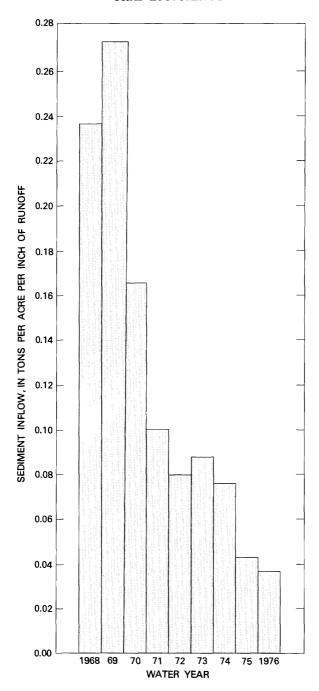


FIGURE 18.—Annual sediment inflow to Lake Bernard Frank per inch of runoff.

Sediment, yield Water year (tons/mi2) (tons/acre) (tons/acre/inch of runoff) 2.36 0.236 .272 2.56 2.45 .165 2.08 .100 2.83 .080 2.16 .088 1.02 .076.98 .043.57 .037

TABLE 11.-Annual sediment yields from total drainage basin of Lake Frank, 1968-76

Table 9 shows that 136,292 tons of sediment entered the impoundment and 5,905 tons of sediment left the impoundment during 1968-76. Trap efficiency, computed from equation 4, is 96 percent.

Estimates of the theoretical trap efficiency of an impoundment are often obtained by the relation between the capacity-inflow (C/I) ratio and trap efficiency as developed by Brune (1953) for normal ponded reservoirs. Normal ponded reservoirs are conventional reservoirs, as contrasted with desilting basins and dry reservoirs.

Average annual inflow to Lake Frank is assumed to equal the 12,300 acre-ft of the average annual outflow for 1968-76. As Lake Frank's capacity is 4,576 acre-ft at the crest of the emergency spillway, the C/I ratio for Lake Frank is 0.37. This gives an estimated trap efficiency of 95 percent from Brune's curve (fig. 19). In this particular instance the measured and theoretical trap efficiencies are almost the same.

Approximately 130,000 tons of sediment is estimated to have accumulated in Lake Bernard Frank during 1968-76. On the basis of a specific dry weight of 59 lb/ft3 (pounds per cubic foot) for the deposits, the total sediment accumulation for the 9-year period was 4,410,000 ft³, or 101 acre-ft. The specific dry weight of the sediment was estimated by procedures outlined by Lara and Pemberton (1963) for Type I reservoir operation and sediment-discharge weighted inflow percentages of 34, 50, and 16 for clay, silt, and sand.

The original sediment-pool capacity (as designed) of the impoundment was 261 acre ft or 11,400,000 ft3. In the 9 year period, 39 percent of the original sediment-pool capacity was lost. This is an average rate of capacity loss of 4.3 percent per year. Assuming

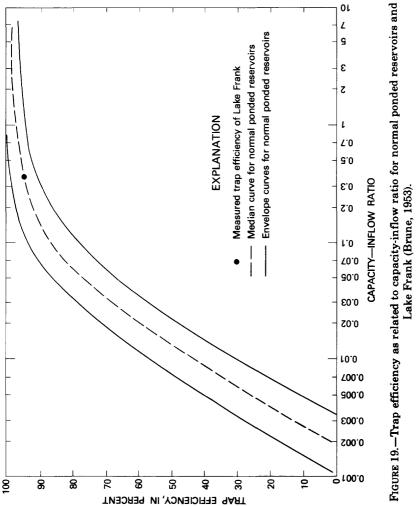


FIGURE 19.—Trap efficiency as related to capacity-inflow ratio for normal ponded reservoirs and

this annual rate of capacity loss, average watershed conditions, and no loss of trap efficiency with a declining C/I ratio, the remaining 61 percent of sediment storage would be utilized in about 14 years. However, table 10 and figure 18 indicate that the annual sediment inflow and annual capacity loss varied from year to year and seemed to be declining in the last several years of the study.

Sediment yield to Lake Frank averaged 0.052 tons per acre per in. of runoff during the 1974-76 water years. This average is considered to be representative of future as well as current yields if no major land use and land cover changes occur in the basin. Mean annual runoff during the 1968-76 water years averaged 18.5 in. The 8,015-acre basin can be expected to yield about 7710 tons (6.0 acre-ft) of sediment annually under average runoff and present land use and land cover conditions. Under such conditions, the remaining 160 acre-ft of the sediment pool will not be fully utilized for 27 years.

SUMMARY AND CONCLUSIONS

Total sediment inflow to Lake Bernard Frank was estimated to be 136,000 tons for the 1968-76 water years. The estimate is based upon measured storm suspended-sediment loads, storm suspended-sediment loads determined from daily sediment-transport curves, suspended-sediment loads based upon land use and land cover in the ungaged part of the study area, and a bedload contribution computed by empirical transport equations. Total sediment inflow was related to land use and land cover changes associated with urbanization in the North Branch Rock Creek basin.

Total sediment outflow from Lake Frank was 5,910 tons during 1968-76. The entire outflow was considered to consist of suspended load with no bedload contribution.

Computations based upon total estimated sediment inflow and measured total sediment outflow indicated a trap efficiency of 96 percent. This agrees closely with the trap efficiency of other impoundments having similar capacity-inflow ratios.

Approximately 39 percent of Lake Frank's sediment-pool capacity has been lost since the dam was closed in 1967. On the basis of recent trends in sediment inflow and average runoff conditions, the sediment pool will be filled in about 27 years.

REFERENCES

- Anttila, P. W., 1970, Sedimentation in Plum Creek subwatershed no. 4, Shelby County, north-central Kentucky: U.S. Geological Survey Water-Supply Paper 1798-G, 54 p.
- Anttila, P. W., and Tobin, R. L., 1978, Fluvial sediment in Ohio: U.S. Geological Survey Water-Supply Paper 2045, 58 p.
- Bailey, J. F., Patterson, J. L., and Paulhus, J. L. H., 1975, Hurricane Agnes, rainfall and floods, June-July 1972: U.S. Geological Survey Professional Paper 924, 403 p.
- Brune, G. M., 1953, Trap efficiency of reservoirs: Transactions of the American Geophysical Union, v. 34, no. 3, p. 407-418.
- Carter, R. W., and Davidian, Jacob, 1968, General procedures for gaging streams: U.S. Geological Survey Techniques Water-Resources Investigations, book 3, chap. A6, 13 p.
- Flint, R. F., 1972a, Fluvial sediment in Hocking River subwatershed 1 (North Branch Hunters Run): U.S. Geological Survey Water-Supply Paper 1798-I, 21 p.

 1972b, Fluvial sediment Salem Fork watershed, West Virginia: U.S. Geological Survey Water-Supply Paper 1798-K, 29 p.
- Guy, H. P., 1973, Laboratory theory and methods for sediment analysis: U.S. Geological Survey Techniques Water-Resources Investigations, book 5, chap. C1, 58 p.
- Guy, H. P., and Norman, V. W., 1970, Field methods for measurement of fluvial sediment: U.S. Geological Survey Techniques Water-Resources Investigations, book 3, chap. C2, 59 p.
- Herb, W. J., and Yorke, T. H., 1976, Storm-period variables affecting sediment transport from urban construction areas: in Proceedings, Third Inter-Agency Sedimentation Conference: U.S. Water-Resources Council Sedimentation Committee, Washington, D.C., p. 1-192.
- Holeman, J. N.,1965, Sedimentation of Loch Raven and Prettyboy Reservoirs, Baltimore County, Maryland: U.S. Department of Agriculture, Soil Conservation Service, SCS-TP-145, 18 p.
- Lara, J. M., and Pemberton, E. L., 1963, Initial unit weight of deposited sediments:
 in Proceedings, Federal Inter-Agency Sedimentation Conference: U.S. Department of Agriculture Miscellaneous Publication 970, p. 818-845.
- Mansue, L. J., and Anderson, P. W., 1974, Effects of land use and retention practices on sediment yields in the Stony Brook basin, New Jersey: U.S. Geological Survey Water-Supply Paper 1798-L, 33 p.
- Montgomery County, Montgomery Soil Conservation District, Maryland-National Capital Park and Planning Commission, 1962, Watershed work plan—Upper Rock Creek watershed, Montgomery County, Maryland: 14 p.
- Mundorff, J. C., 1968, Fluvial sediment in the drainage area of K-79 Reservoir, Kiowa Creek basin, Colorado: U.S. Geological Survey Water-Supply Paper 1798-D, 26 p.
- Porterfield, George, 1972, Computation of fluvial-sediment discharge: U.S. Geological Survey Techniques Water-Resources Investigations, book 3, chap. C3, 66 p.
- Sheppard, J. R., 1960, Investigation of Meyer-Peter, Muller bedload formulas: U.S. Bureau of Reclamation, 22 p.
- Shulits, Sam, 1935, The Schoklitsch bedload formula: Engineering, v. 139, p. 644-646, 687.
- Yorke, T. H., and Herb, W. J., 1978, Effects of urbanization on streamflow and sediment transport in the Rock Creek and Anacostia River basins, Montgomery County, Maryland, 1962-74: U.S. Geological Survey Professional Paper 1003, 71 p.